

FIG. 2

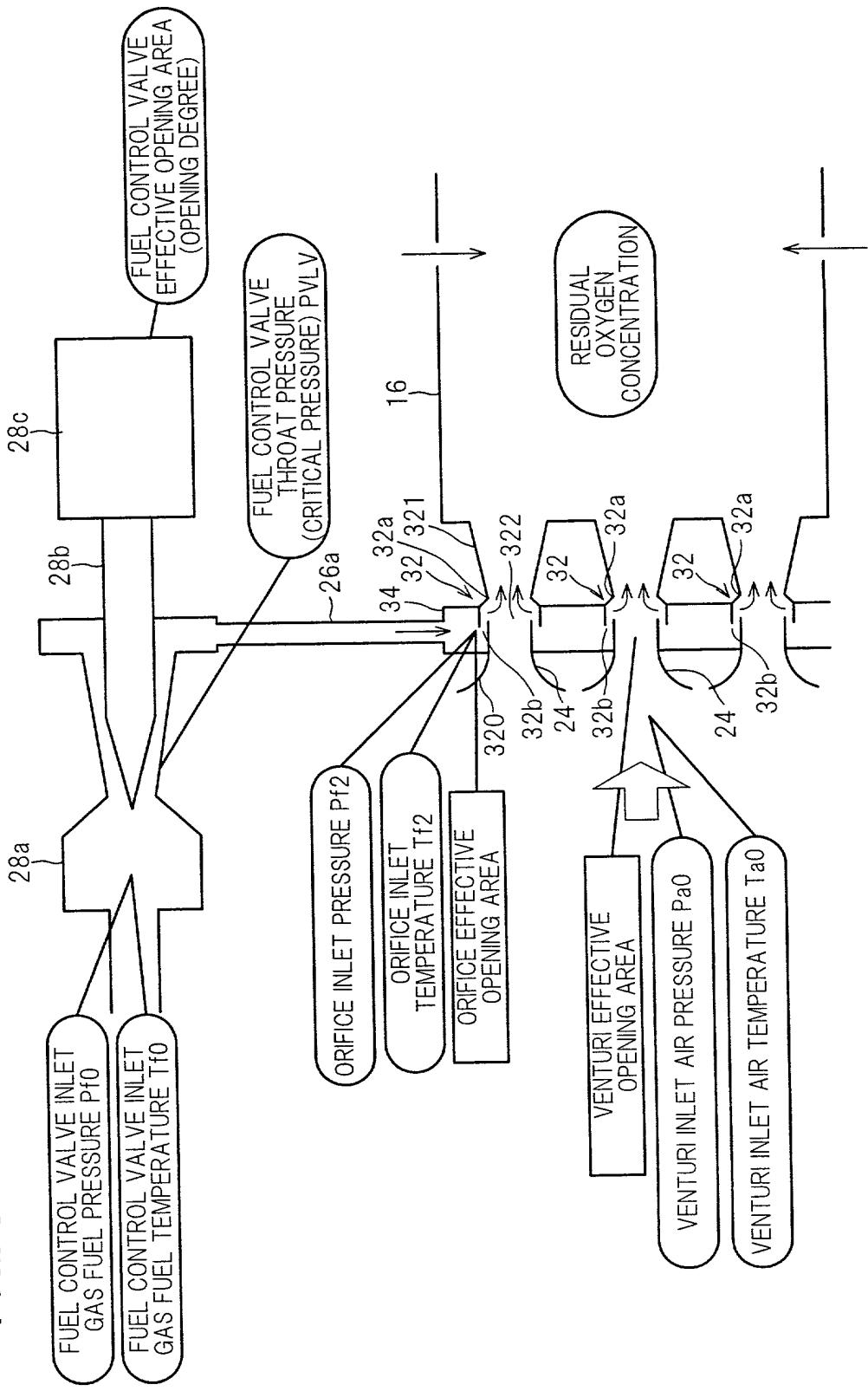


FIG. 3

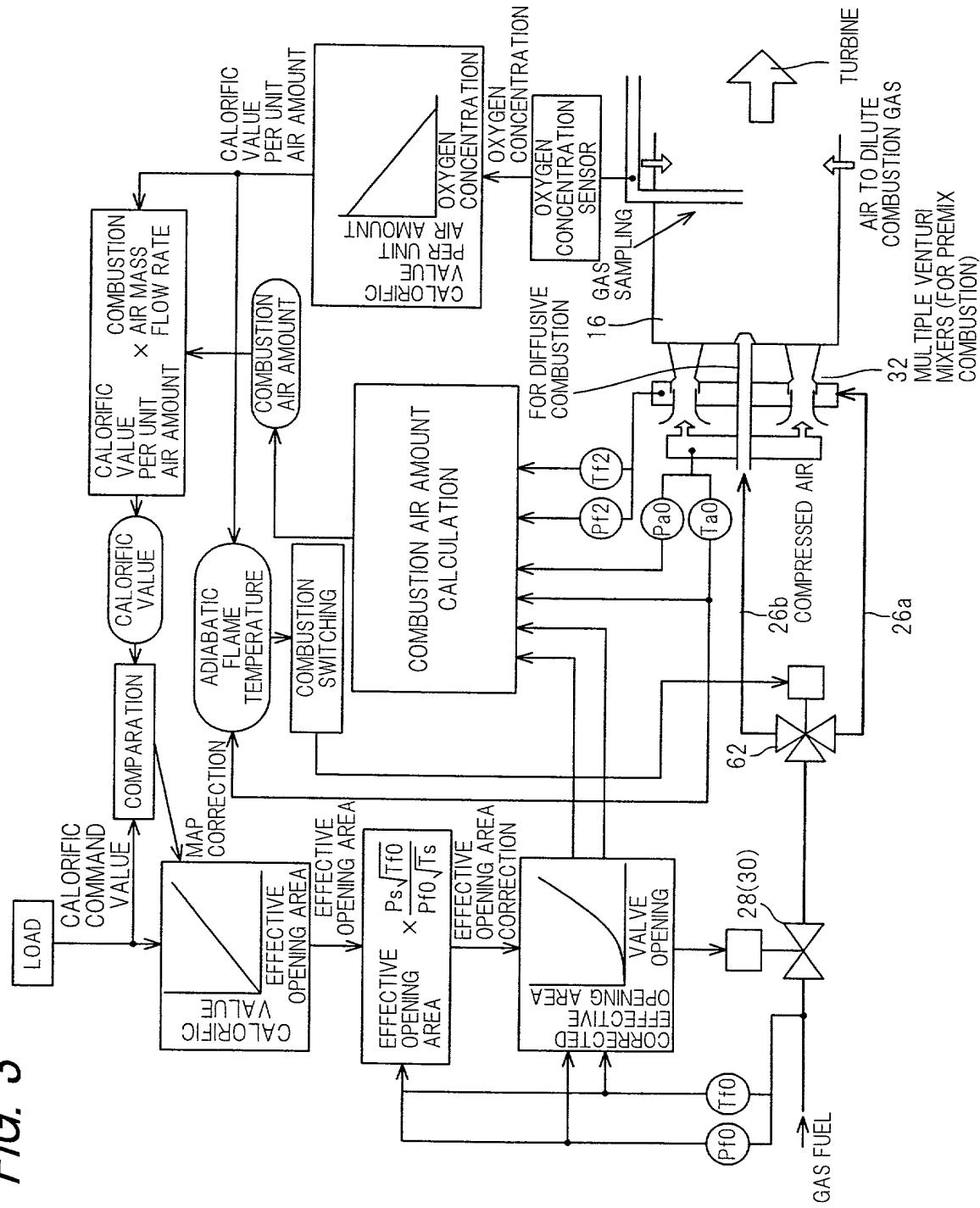
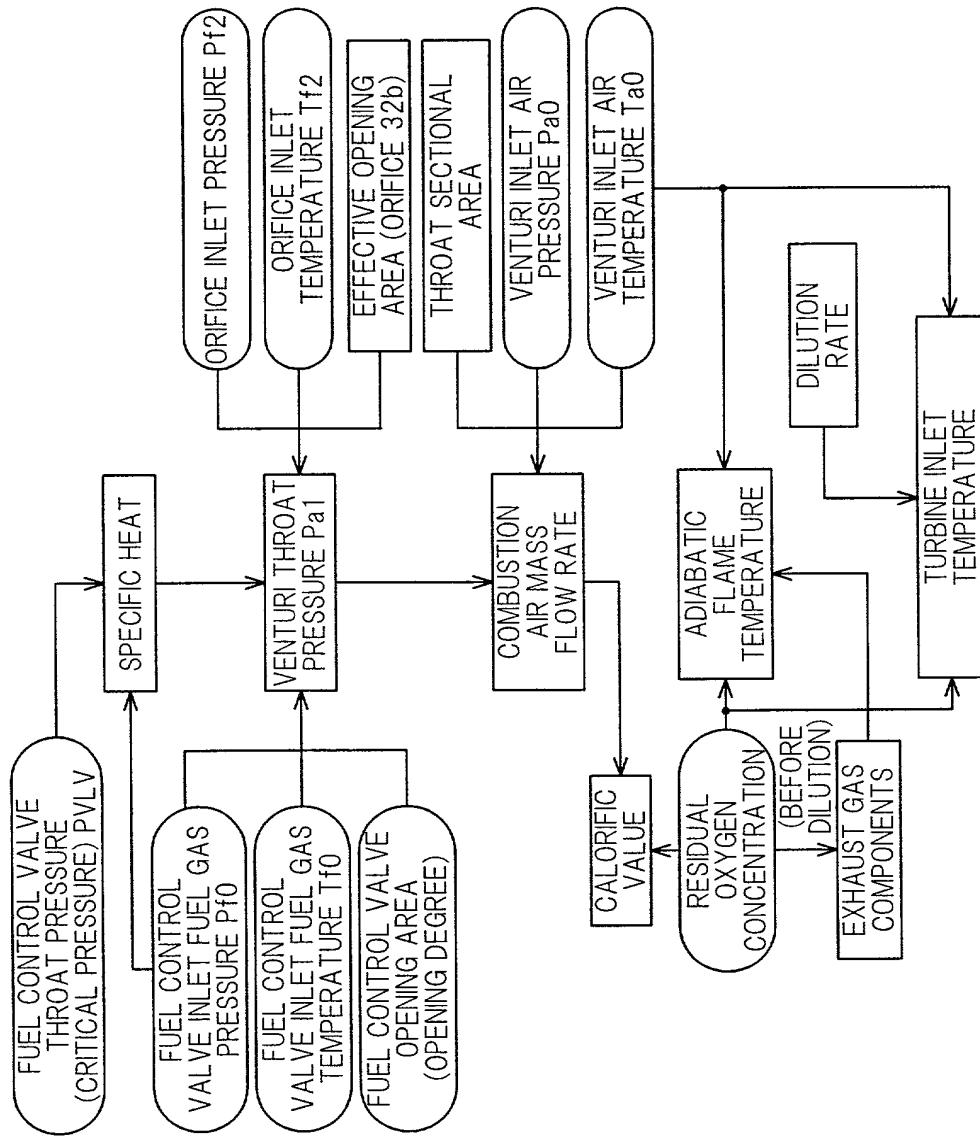


FIG. 4



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FIG. 5

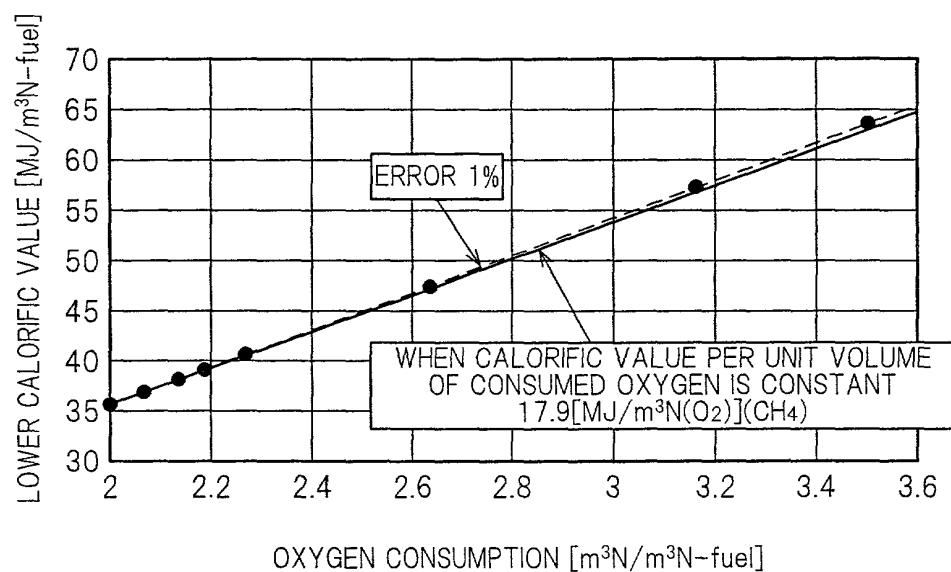


FIG. 6

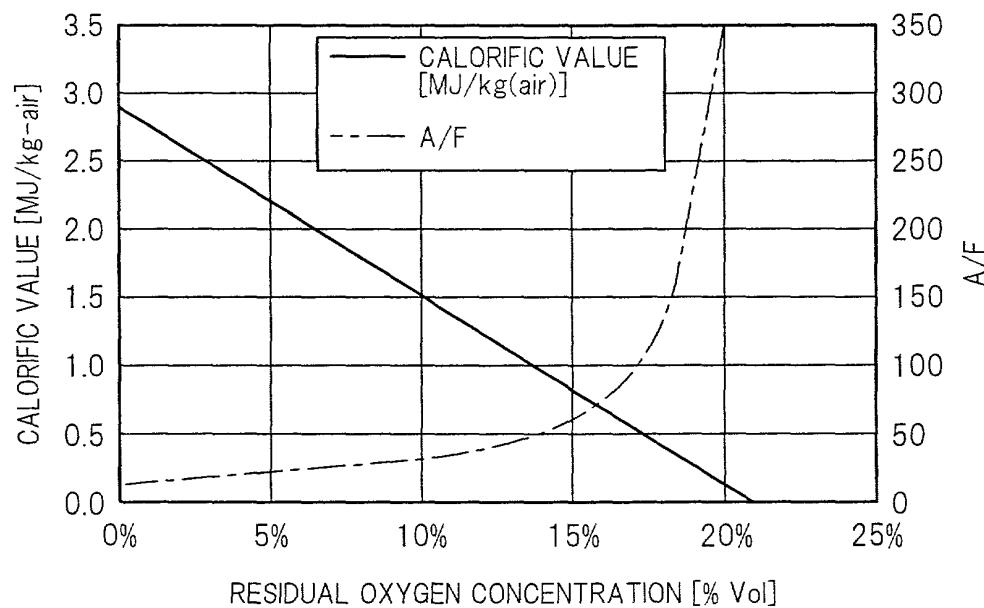
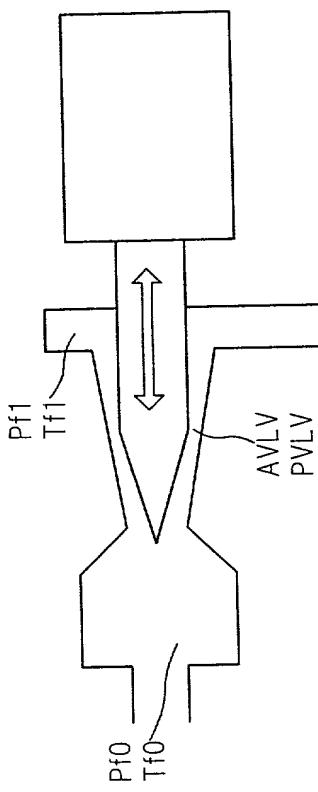


FIG. 7



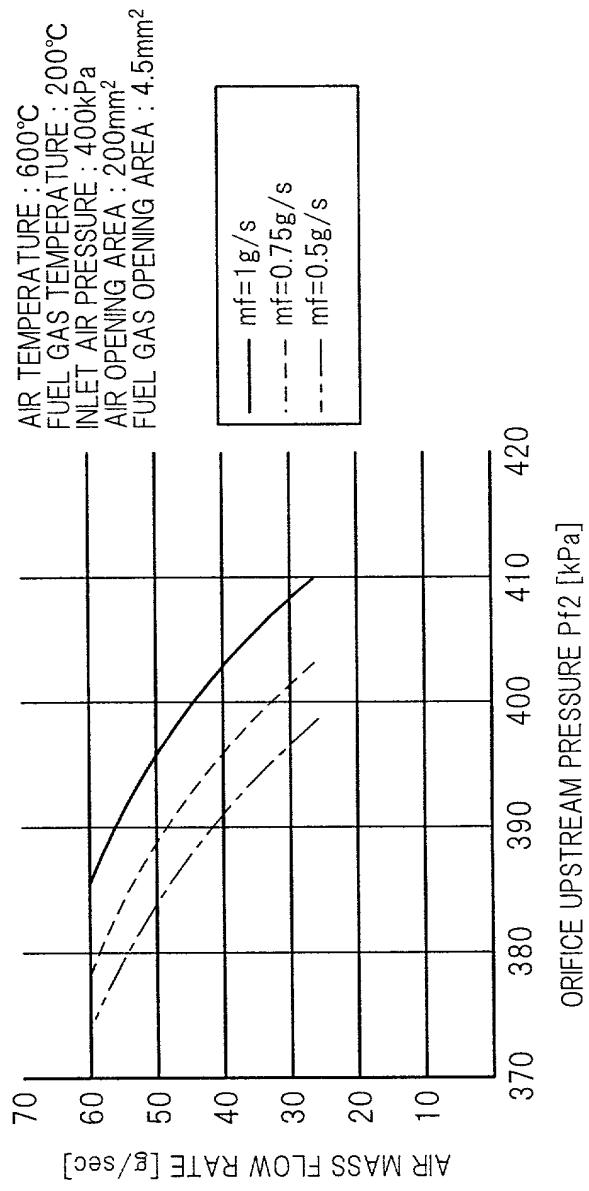
$$mf = \frac{P_f 2 A_f}{\sqrt{R_f T_f 2}} \sqrt{\frac{2 \kappa_f}{\kappa_{f-1}} \left\{ \left( \frac{P_{a1}}{P_f 2} \right)^{\frac{2}{\kappa_f}} - \left( \frac{P_{a1}}{P_f 2} \right)^{\frac{\kappa_f + 1}{\kappa_f}} \right\}}$$

$$ma = \frac{P_{a0} A_a}{\sqrt{R_a T_{a0}}} \sqrt{\frac{2 \kappa_a}{\kappa_{a-1}} \left\{ \left( \frac{P_{a0}}{P_{a1}} \right)^{\frac{2}{\kappa_a}} - \left( \frac{P_{a0}}{P_{a1}} \right)^{\frac{\kappa_a + 1}{\kappa_a}} \right\}}$$

P<sub>f0</sub> : FUEL CONTROL VALVE INLET PRESSURE [Pa]  
 P<sub>f2</sub> : ORIFICE INLET PRESSURE [Pa]  
 P<sub>V1</sub> : FUEL CONTROL VALVE THROAT PRESSURE [Pa]  
 P<sub>a0</sub> : VENTURI INLET AIR PRESSURE [Pa]  
 P<sub>a1</sub> : VENTURI THROAT PRESSURE [Pa]  
 T<sub>f0</sub> : FUEL CONTROL VALVE INLET TEMPERATURE [K]  
 T<sub>f2</sub> : ORIFICE INLET TEMPERATURE [K]  
 T<sub>a0</sub> : VENTURI INLET AIR TEMPERATURE [K]

mf : FUEL MASS FLOW RATE [kg/sec]  
 ma : AIR MASS FLOW RATE [kg/sec]  
 AVL<sub>V</sub> : FUEL CONTROL VALVE EFFECTIVE OPENING AREA [m<sup>2</sup>]  
 Af : ORIFICE INLET EFFECTIVE OPENING AREA [m<sup>2</sup>]  
 Aa : VENTURI THROAT EFFECTIVE OPENING AREA [m<sup>2</sup>]  
 R<sub>f</sub> : FUEL GAS CONSTANT [kJ/kg K]  
 R<sub>a</sub> : AIR GAS CONSTANT [kJ/kg K]  
 κ<sub>f</sub> : FUEL GAS SPECIFIC HEAT  
 κ<sub>a</sub> : AIR SPECIFIC HEAT

FIG. 8



## FIG. 9

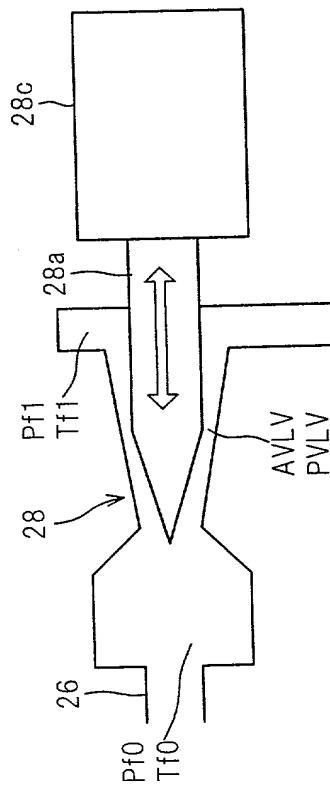
$$mf_v = \frac{Pf0 AVLV}{\sqrt{RTf0}} M \sqrt{\kappa_f} \left( 1 + \frac{\kappa_{f-1}}{2} M^2 \right)^{\frac{\kappa_{f+1}}{2(\kappa_{f-1})}}$$

$$mf_0 = \frac{Pf2 A_f}{\sqrt{RTf2}} \sqrt{\left[ \frac{2 \kappa_f}{\kappa_{f-1}} \left\{ \left( \frac{P_{a1}}{P_{f2}} \right) \frac{2}{\kappa_f} - \left( \frac{P_{a1}}{P_{f2}} \right) \frac{\kappa_{f+1}}{\kappa_f} \right\} \right]}$$

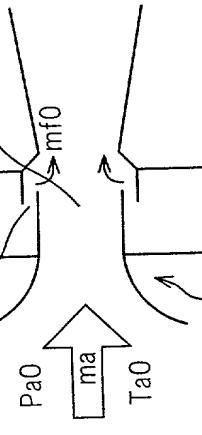
SINCE VALVE IS CHOKE-FLOW RATE VALVE,  
MACH IS 1, THIS YIELDS FOLLOWING

$$= \left\{ \frac{Pf0 AVLV \sqrt{f f2}}{\sqrt{f0} Pf2 A_f} \sqrt{\kappa_f} \left( 1 + \frac{\kappa_{f-1}}{2} \right)^{\frac{\kappa_{f+1}}{2(\kappa_{f-1})}} \right\}$$

$$ma = \frac{Pa0 A_a}{\sqrt{Ra Ta0}} \sqrt{\left[ \frac{2 \kappa_a}{\kappa_{a-1}} \left\{ \left( \frac{Pa0}{Pa1} \right) \frac{2}{\kappa_a} - \left( \frac{Pa0}{Pa1} \right) \frac{\kappa_{a+1}}{\kappa_a} \right\} \right]}$$



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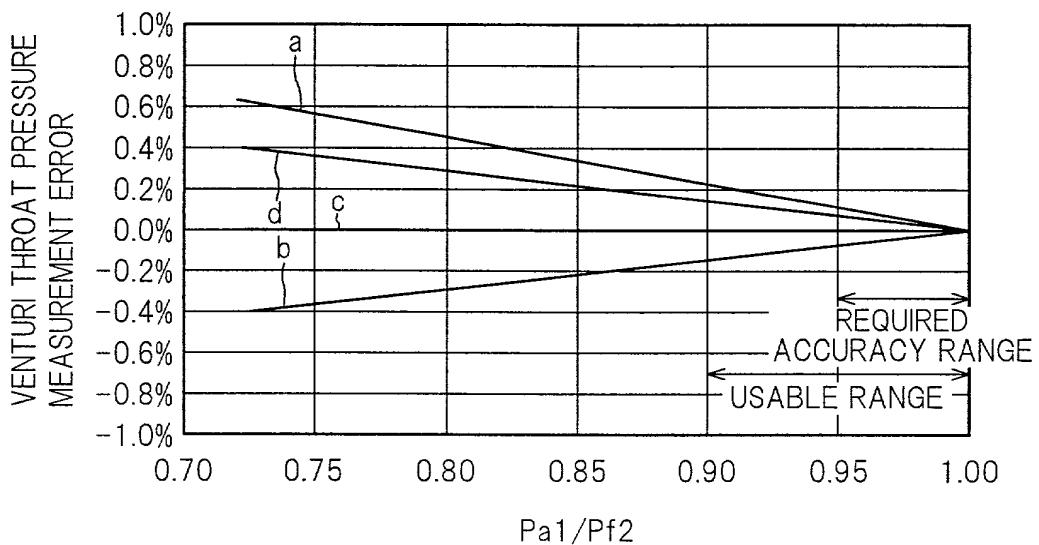


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$Pf0$  : FUEL CONTROL VALVE INLET PRESSURE [Pa]  
 $Pf2$  : ORIFICE INLET PRESSURE [Pa]  
 $PVLV$  : FUEL CONTROL VALVE THROAT PRESSURE [Pa]  
 $Pa0$  : VENTURI INLET AIR PRESSURE [Pa]  
 $Pa1$  : VENTURI THROAT PRESSURE [Pa]  
 $Tf0$  : FUEL CONTROL VALVE INLET TEMPERATURE [K]  
 $Tf2$  : ORIFICE INLET TEMPERATURE [K]  
 $Ta0$  : VENTURI INLET AIR TEMPERATURE [K]

$mf$  : FUEL MASS FLOW RATE [kg/sec]  
 $ma$  : AIR MASS FLOW RATE [kg/sec]  
 $AVLV$  : FUEL CONTROL VALVE EFFECTIVE OPENING AREA [ $m^2$ ]  
 $Af$  : ORIFICE INLET EFFECTIVE OPENING AREA [ $m^2$ ]  
 $A_a$  : VENTURI THROAT EFFECTIVE OPENING AREA [ $m^2$ ]  
 $R_f$  : FUEL GAS CONSTANT [ $\text{kJ}/\text{kg K}$ ]  
 $R_a$  : AIR GAS CONSTANT [ $\text{kJ}/\text{kg K}$ ]  
 $\kappa_f$  : FUEL GAS SPECIFIC HEAT  
 $\kappa_a$  : AIR SPECIFIC HEAT

FIG. 10



SAMPLES	SPECIFIC HEAT
a	1.309
b	1.251
c	1.274
d	1.296

FIG. 11

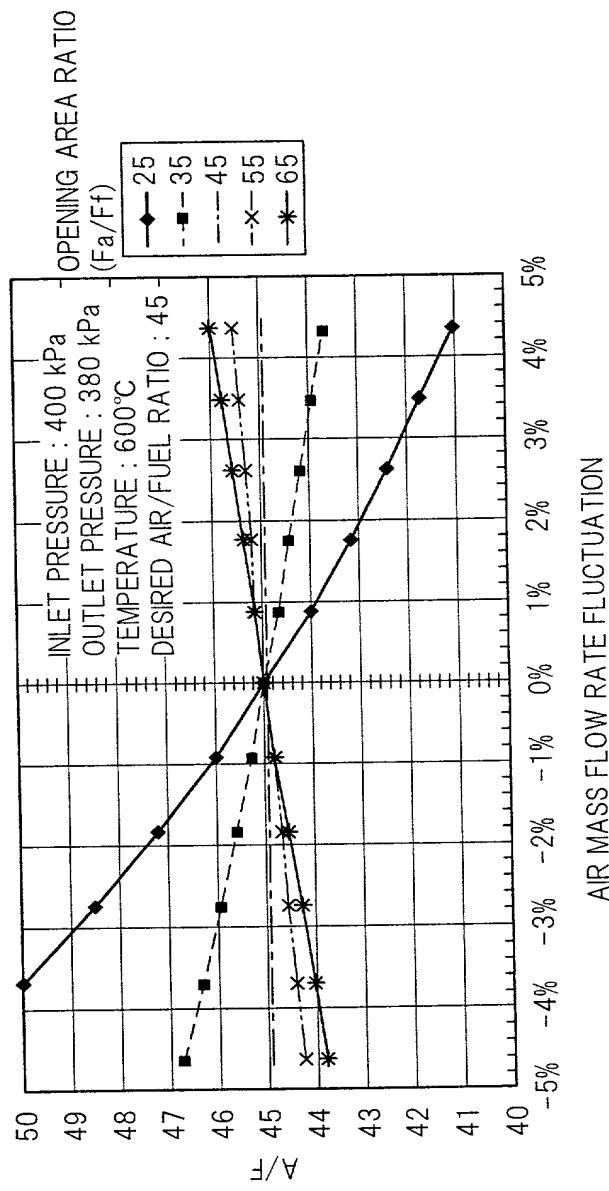


FIG. 12

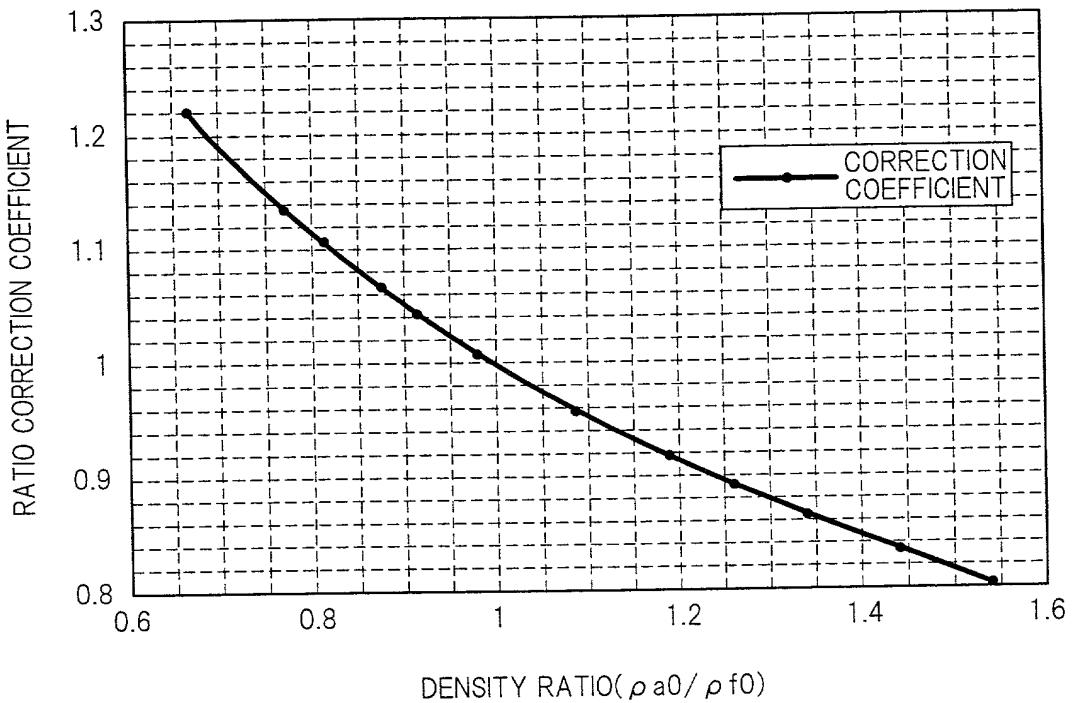


FIG. 13

